

Forces and moments generated by removable thermoplastic aligners: Incisor torque, premolar derotation, and molar distalization

Mareike Simon,^a Ludger Keilig,^b Jörg Schwarze,^c Britta A. Jung,^d and Christoph Bourauel^e Freiburg, Bonn, and Cologne, Germany

Introduction: The exact force systems as well as their progressions generated by removable thermoplastic appliances have not been investigated. Thus, the purposes of this experimental study were to quantify the forces and moments delivered by a single aligner and a series of aligners (Invisalign; Align Technology, Santa Clara, Calif) and to investigate the influence of attachments and power ridges on the force transfer. Methods: We studied 970 aligners of the Invisalign system (60 series of aligners). The aligners came from 30 consecutive patients, of which 3 tooth movements (incisor torque, premolar derotation, molar distalization) with 20 movements each were analyzed. The 3 movement groups were subdivided so that 10 movements were supported with an attachment and 10 were not. The patients' ClinCheck (Align Technology, Santa Clara, Calif) was planned so that the movements to be investigated were performed in isolation in the respective quadrant. Resin replicas of the patients' intraoral situation before the start of the investigated movement were taken and mounted in a biomechanical measurement system. An aligner was put on the model, the force systems were measured, and the calculated movements were experimentally performed until no further forces or moments were generated. Subsequently, the next aligners were installed, and the measurements were repeated. Results: The initial mean moments were about 7.3 N·mm for maxillary incisor torque and about 1.0 N for distalization. Significant differences in the generated moments were measured in the premolar derotation group, whether they were supported with an attachment (8.8 N·mm) or not (1.2 N·mm). All measurements showed an exponential force change. Conclusions: Apart from a few maximal initial force systems, the forces and moments generated by aligners of the Invisalign system are within the range of orthodontic forces. The force change is exponential while a patient is wearing removable thermoplastic appliances. (Am J Orthod Dentofacial Orthop 2014;145:728-36)

he Invisalign system, introduced by Align Technology (Santa Clara, Calif) in 1999, combines the basic principles of Kesling's, Ponitz's, McNamara's, and Sheridan's orthodontic treatment with removable thermoplastic appliances (RTAs; appliances made from transparent plastic material such as polyurethane) with

^aOrthodontist, Department of Orthodontics, University Hospital of Freiburg, Freiburg, Germany; doctoral candidate, Department of Oral Technology, School of Dentistry, University of Bonn, Bonn, Germany.

^bSenior scientist, Department of Oral Technology, School of Dentistry, University of Bonn, Bonn, Germany.

^eProfessor and head, Orthodontics Department, School of Dentistry, University of Bonn, Bonn, Germany.

Each author completed an ICMJE form for the disclosure of potential conflicts of interest and the following was reported. This study was supported by the Clear Aligner Research Award from Align Technology. No other conflicts were reported. Address correspondence to: Mareike Simon, Hugstetter Str 55, 79106 Freiburg, Germany: e-mail. mareike.simon@uniklinik-freiburg.de.

Submitted, August 2013; revised and accepted, March 2014. 0889-5406/\$36.00

Copyright © 2014 by the American Association of Orthodontists. http://dx.doi.org/10.1016/j.ajodo.2014.03.015 modern CAD-CAM stereolithography and tooth movement simulation software. Since it is a relatively new method, some aspects are still insufficiently investigated. Most previous studies on RTAs are case reports and system descriptions. Furthermore, material science studies have evaluated the changes in force delivery properties of RTAs after thermocycling, as well as the chemical and morphologic changes after usage. ⁷⁻⁹

Forces and moments generated by RTAs have barely been investigated.

In 3 follow-up in-vitro studies, Hahn et al¹⁰⁻¹² quantified the forces for 3 tooth movements (rotation, tipping, and torque of a maxillary central incisor) generated by 3 thermoplastic materials (Ideal Clear [Dentsply GAC, Gräfelfing, Germany], Erkodur [Erkodent Erich Kopp GmbH, Pfalzgrafenweiler, Germany], and Biolon [Dreve Dentamid GmbH, Unna, Germany]). They all had a thickness of 1.0 mm but differed in the thermoforming process. Regarding their results, it seems that pressure-formed appliances exert greater force systems at higher rates of activation compared with

^cPrivate practice, Cologne, Germany.

^dProfessor and head of clinic, Department of Orthodontics, University Hospital of Freiburg, Freiburg, Germany.

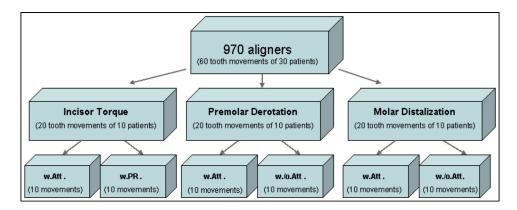


Fig 1. On the basis of the tooth movement to be analyzed, participating patients were divided in 3 main groups (incisor torque, premolar derotation, molar distalization). To determine the influence of auxiliaries to the force transfer, 2 subgroups were made in each main group: in 1 subgroup the movement was performed with an attachment (*w.Att.*), and in the other subgroup no attachment was used (*w./o.Att.*), except incisor torque, where power ridges were used (*w.PR.*). The attachments used in each group were "horizontal ellipsoid attachment" for maxillary incisor torque (group 1), "optimized rotation attachment" for premolar derotation (group 2), and "horizontal beveled gingival attachment" for molar distalization (group 3).

thermoplastic vacuum-formed appliances. However, the results were statistically significant only in some cases.

In an in-vivo study, Barbagallo et al¹³ investigated the force transmitted by aligners (synonym for RTAs) of the ClearSmile system (Clear Smile appliance, Woollongong, Australia) using Pressurex films (Fuji Photo Film Co, Ltd, Tokyo, Japan). The films, placed under the aligners, recorded the overall mean forces. The measurements were performed on the first day and after 2 weeks—the last day of wearing the aligner. They found a high initial mean force on the first day and a low final force, and concluded that the force curve is not linear but, rather, exponential. Their results agree with the findings of Vardimon et al, 14 who indirectly evaluated the generated forces of aligners of the Invisalign system. Assuming that forces generated by aligners behave like the von Mises strains developed in an aligner, they bonded strain gauge rosettes on aligner surfaces and measured in-vivo strains during Invisalign treatment. Their results showed a peak strain on the first day followed by a plateau phase at a lower force level between days 2 and 15.

The main disadvantages of these in-vivo studies are that the data only show an overall mean force on a specific position on the crown at a certain time. The exact force systems in all 3 planes of space, as well as the exact distribution of the forces and moments, have not been detected so far, but they are important to know when planning orthodontic treatment with an aligner system.

Thus, the aims of this experimental study were (1) to quantify the exact initial force systems that are delivered by an individual aligner, (2) to measure the force systems generated by a series of aligners, and (3) to investigate the influence of auxiliaries (attachments, power ridges) on the force transfer.

These aims were achieved by aligners of the Invisalign system for 3 predefined tooth movements, since these are the movements described as impossible or difficult to perform with RTAs: incisor torque, premolar derotation, and molar distalization. 15-17

MATERIAL AND METHODS

In this study, we investigated the initial force systems delivered by 970 individual aligners and 60 series of aligners (mean aligners per series, 16.7; SD, 5.0). These aligners came from 30 consecutive patients (11 male, 19 female; ages, 13-72 years; mean age, 32.9 years; SD, 16.3 years) who underwent orthodontic treatment in 2011 and 2012 in a private orthodontic practice in Cologne, Germany. Our inclusion criteria for the patients were orthodontic treatment with Invisalign aligners and a need for 1 of these 3 movements: incisor torque, premolar derotation, or molar distalization. Exclusion criteria were cleft lip and palate or any other syndrome-associated orofacial malformation.

According to the investigated tooth movement, the 30 patients were divided into 3 main movement categories with 10 patients in each group. In each movement category, 20 tooth movements (2 per patient) were determined. To investigate the influence of auxiliaries such as attachments (temporarily bonded composite buttons) and power ridges (pressure lines close to the gingival margin), the 3 main movement categories were split into 2 subgroups using a split-mouth design (Fig 1).

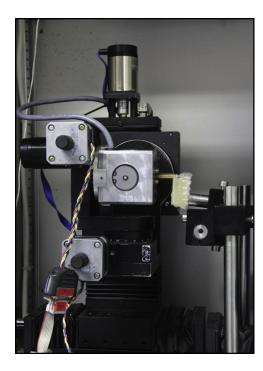


Fig 2. Experimental setup: a resin replica with an aligner is mounted in the orthodontic measurement and simulation system. The tooth to be analyzed is connected to 1 of the 2 computer-controlled 3-dimensional sensors. The measured forces and moments are registered by the sensor, and the motor-driven positioning table simulates the respective tooth movement.

In group 1, maxillary central incisor torque was greater than 10°, supported by a "horizontal ellipsoid attachment" or power ridges.

In group 2, premolar derotation was greater than 10° , supported by an "optimized rotation attachment" or with no auxiliary.

In group 3, molar distalization was greater than 1.5 mm, supported by a 4-mm-long "horizontal beveled gingival attachment" or with no auxiliary.

The force systems generated by the series of 60 aligners for 60 tooth movements from 30 patients (2 tooth movements per patient, 20 tooth movements in each main group, and 10 tooth movements in each subgroup) were determined.

All the attachments we used were engineered by Align Technology to achieve predictable tooth movements. The vertical and transverse positions of the attachments on the tooth surfaces were done according to Align Technology's treatment protocol (for incisor torque and molar distalization) or automatically by the software (for premolar derotation).¹⁷ The allocations of the teeth to the subgroups with or without an auxiliary were randomized.

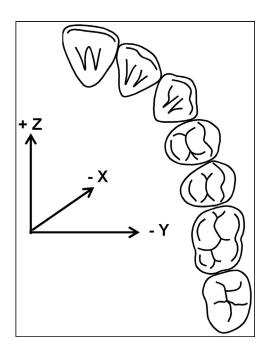


Fig 3. Definitions of the tooth axes.

Using ClinCheck (Align Technology, Santa Clara, Calif), the treatment was planned so that the tooth movement to be investigated was performed in isolation at the beginning of the treatment to make it clearly distinguishable from any other tooth movement.

The experimental investigation of the force systems generated by the aligners was performed at the University of Bonn in Germany. Alginate impressions (Tetrachrom Alginat; Kaniedenta, Herford, Germany) of each patient's intraoral situation before tooth movement were taken, and plaster cast models were produced (Snow White Plaster; Kerr, Karlsruhe, Germany). Thereafter, resin replicas (Palavit G; Heraeus Kulzer, Hanau, Germany) of the pretreatment plaster cast models were produced, and the tooth to be analyzed was removed from the replica. Both the resin replica of the whole arch and the tooth to be moved were mounted into the orthodontic measurement and simulation system (Fig 2). This is a custom-made system developed for orthodontic biomechanical investigations. More details of the technical specifications and the software running the experiments can be found in several articles. 18,19 The measuring system consists of 2 force and moment sensors that can measure force and moment vectors in all 3 dimensions (x, y, and z). Sensors are mounted on a motor-driven 6-axis positioning table that can perform full 3-dimensional movements. The removed tooth was connected to 1 sensor, and the dental arch was mounted in the orthodontic measurement and simulation system. Adjustments were made with a passive aligner of the

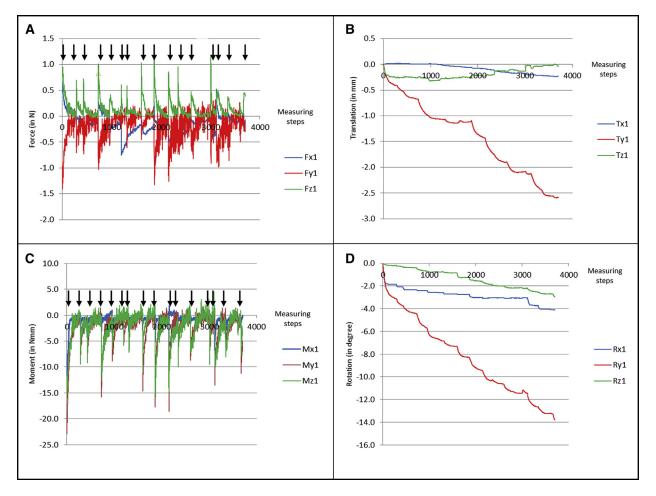


Fig 4. Representative orthodontic measurement and simulation system measurements of 15 aligners of the forces, moments, translation, and rotation of a maxillary incisor torque movement with power ridge: **A**, forces generated by the aligners in all 3 axes; **B**, resulting simulated translational tooth movement; **C**, measured torque movement in all 3 axes; **D**, resulting simulated rotations (*arrows*, time points for insertion of new aligners).

Table I. Results of t test, $P \le 0.05$, for all forces and moments						
Force or moment	Molar distalization	Incisor torque	Premolar derotation			
Fx	0.06	0.26	0.01			
Fy	0.02	0.00	0.00			
Fz	0.00	0.03	0.38			
Mx	0.00	0.00	0.00			
My	0.00	0.03	0.00			
Mz	0.10	0.00	0.00			

initial stage so that the tooth under investigation was in its initial position in the dental arch, and no active force system was transferred to the tooth. Subsequently, a duplicate of the clinically used aligner series was placed on the model, the removed tooth was deflected, and the forces and moments generated by the aligner were measured by the orthodontic measurement and simulation system sensor.

Based on the force system, the control program of the orthodontic measurement and simulation system calculated the developed tooth movement using a mathematical model, taking into consideration the center of resistance of the tooth. According to the literature, this is defined as one-third of the root length from the alveolar crest to the apex and at the furcation for the maxillary molars.²⁰

Tooth movement was implemented in increments and transformed by the stepping motors of the positioning tables. Depending on the vector of movement, the absolute value of each movement increment was below 0.1 mm. Single components were typically even

Table II. Forces and moments with and without attachment/power ridge

Movement	Mean initial force or moment*	SD of initial force or moment	Mean initial vertical force (Fz)	Mean movement peraligner [†]
Premolar derotation w Att	8.8 N·mm	5.6	−0.2 N	1.1°
Premolar derotation w/o Att	1.2 N·mm	1.9	−0.5 N	1.2°
Distalization w Att	−1.1 N	0.8	−0.7 N	0.2 mm
Distalization w/o Att	−0.8 N	0.7	−0.5 N	0.2 mm
Incisor torque w Att	6.7 N·mm	5.1	0.2 N	1.2°
Incisor torque w PR	7.9 N·mm	4.7	0.1 N	1.1°

w Att, With attachment; w/o Att, without attachment; PR, power ridge.

*Mean initial force or moment corresponds to the direction of movement: premolar derotation (Mx), distalization (Fz), or incisor torque (My); †Mean movement per aligner corresponds to the direction of movement according to ClinCheck.

close to zero (<0.01 mm). By means of continuous measurements of the force systems and simulation of the resulting tooth movement, the force progression generated by an aligner was measured, and the experimentally resulting tooth movement was depicted. For all 3 types of tooth movements, the measurements were terminated when forces dropped below 0.2 N (1 N = $1/9.81 \, \text{kg} = 102 \, \text{g}$). Then the next aligner of the series was used. On average, 17 aligners were used to perform each tooth movement. Sixty tooth movements from 30 patients were investigated, so that 970 aligners were investigated in this study. To compensate for interlaboratory measuring inaccuracies, the measurements were repeated at least 3 times; overall, 2910 measurements were performed.

To describe the tooth movements in all 3 spatial dimensions, a coordinate system was set up: the positive x-axis describes extrusive and the negative x-axis describes intrusive forces and movements, parallel to the long axis of the tooth. Horizontal forces and movements are described in the y-axis and the z-axis. In respect to the position of the tooth in the dental arch, the y-axis and the z-axis describe different movements for a molar and an incisor. For a molar, the positive y-axis describes buccal movements, the negative y-axis describes palatinal and lingual forces and movements, the positive z-axis describes mesial movements, and the negative zaxis describes distal forces and movements. For a maxillary incisor, the positive y-axis describes distal movements, the negative y-axis describes mesial forces and movements, the positive z-axis describes buccal movements, and the negative z-axis describes lingual forces and movements (Fig 3). Thus, the biomechanical measured force systems could be transferred exactly to the generated tooth movement.

Statistical analysis

In this study, we investigated the force systems of 970 Invisalign aligners from 30 consecutively recruited patients. The aligners were produced to perform 3

predefined tooth movements: incisor torque, premolar derotation, and molar distalization. In all, 60 tooth movements (2 movements in each patient, 20 movements in each group) were determined. A split-mouth design was used to investigate the influence of auxiliaries (attachments and power ridges) on the force transfer. Therefore, the 3 main groups were divided into 2 subgroups (with an attachment, and with no attachment or with a power ridge), to which the teeth were allocated randomly.

The analysis included a comparison of the initial force systems that were delivered by an individual aligner and by a series of aligners. The statistical evaluation included the analysis of the measured force systems as well as minimums, maximums, means, and standard deviations of the means. Since the results were normally distributed according to a chi-square test, statistical significance was performed using the t test with a significance level of $P \leq 0.05$.

RESULTS

Figure 4 shows an example of a typical maxillary incisor torque measurement of 15 aligners with the measured forces (Fig 4, A), the corresponding translational movements (Fig 4, B), the measured moments (Fig 4, C), and the resulting rotational movements (Fig 4, D) each in all 3 axes. The data clearly demonstrate that each aligner creates high initial forces, followed by an exponential decrease to forces or moments just above 0 N/N·mm. Furthermore, the data demonstrate that the forces and moments between consecutive aligners differ, even though a continuous movement was planned in ClinCheck.

Regarding the influence of auxiliaries (attachments, power ridges) to the force transfer, the results show that distalization and derotation supported by an attachment and incisor torque supported by a power ridge have higher forces or moments corresponding to the direction of movement. In nearly all cases, the differences were statistically significant (Table I). Moreover, with an attachment,

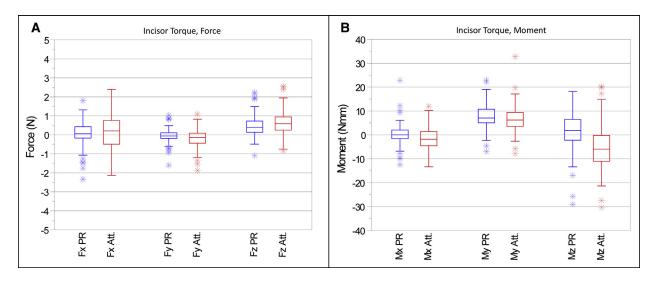


Fig 5. Box plots comparing the results of the initial **A**, forces (Fx, Fy, Fz) and **B**, moments (Mx, My, Mz) between power ridge and attachment measurements for incisor torque. The *boundaries* of the boxes represent 25% and 75% values; the *lines* in the boxes represent the median values. *Vertical bars* of *lines* connected to boxes indicate the lowest datum still within 1.5 interquartile range of the lower quartile and the highest datum still within 1.5 interquartile range of the upper quartile. Outliers are plotted with *stars*.

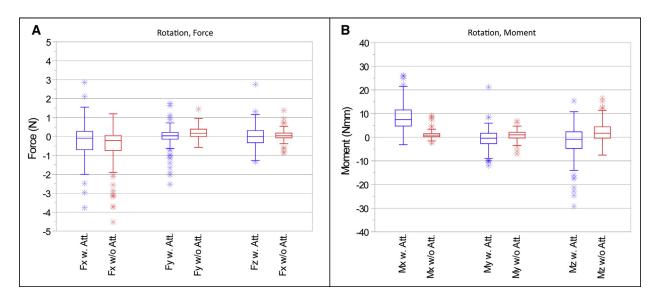


Fig 6. Box plots comparing the results of the initial **A**, forces (Fx, Fy, Fz) and **B**, moments (Mx, My, Mz) between attachments and nonattachment measurements for premolar derotation.

the intrusive forces were reduced in the premolar derotation and incisor torque groups (Table 11).

The results show the initial mean moments (My) in the maxillary incisor torque group to be 7.9 N·mm with power ridges and 6.7 N·mm with an attachment. In both subgroups, the mean vertical force was slightly extrusive (with an attachment, 0.2 N; supported by a power ridge, 0.1 N). The results of the comparison of

all forces and moments of the measurements with power ridges and attachments are shown in Figure 5. According to ClinCheck data, movements between 12° and 30° were planned with average stagings of 1.1° per aligner for movements supported by power ridges and 1.2° per aligner for movements supported by an attachment.

Substantial differences of the measured moments were observed in the premolar derotation group. With

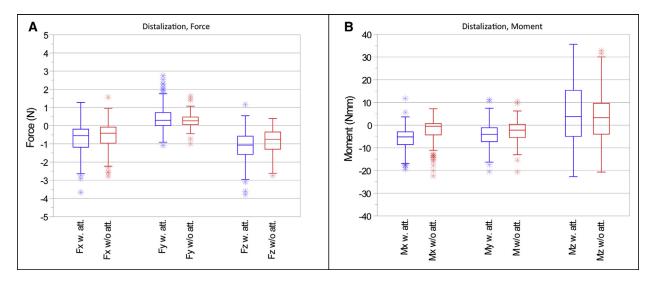


Fig 7. Box plots comparing the results of the initial **A**, forces (Fx, Fy, Fz) and **B**, moments (Mx, My, Mz) between attachments and nonattachment measurements for molar distalization.

an attachment, the initial mean moment for derotation (Mx) was 8.8 N·mm with a mean vertical force of -0.2 N. Without an attachment, the initial mean moment was only 1.2 N·mm, but the initial mean vertical force increased to -0.5 N. The corresponding box plots are given in Figure 6. According to ClinCheck, the total amount of derotation ranged between 12° and 35° . The staging for the movements with an attachment was between 0.5° and 1.3° per aligner; on average, it was 1.1° per aligner. Without an attachment, the amount of derotation per aligner was between 0.4° and 2.1° ; on average, it was 1.2° per aligner.

In the distalization group, the initial mean forces in the direction of movement (Fz) were -1.1 N with an attachment and -0.8 N without an attachment. The mean vertical forces were intrusive: -0.7 N with an attachment and -0.5 N without an attachment (Fig 7). The differences were not statistically significant (P > 0.06). According to ClinCheck data, movement distances between 1.5 and 3.9 mm were performed: on average, the movement was 2.6 mm with an average staging of 0.2 mm per aligner.

DISCUSSION

The exact force systems and their progressions generated by Invisalign aligners have not been investigated until now. Thus, the overall aims of this study were to determine the exact forces and moments (Fx, Fy, Fz, Mx, My, Mz) and to investigate the influence of an attachment or power ridge on the force transfer

of 3 predefined tooth movements (maxillary incisor torque, premolar derotation, and maxillary molar distalization).

As shown in a systematic literature review by Ren et al,²¹ no evidence-based optimal orthodontic force level can be determined.

In our experimental setup, we found mean initial moments for maxillary incisor torque between 6.7 and 7.9 N·mm, about 1 N for molar distalization, and between 1.2 and 8.8 N·mm for premolar derotation. Altogether, the measured forces and moments correspond with values in the literature for these tooth movements.²¹ In the premolar derotation group, the measured moments differed significantly, depending on whether an attachment was used. This indicates that load transfer from an aligner to a cylindric tooth without an attachment is possible only to a limited extent. The results correspond to the reports in the literature, where the derotation of cylindric teeth is described as one of the most critical movements to be achieved with RTAs.²² With the exception of the distalization measurements, all attachments seemed to reduce the intrusive tendency of the teeth. The exact influence of the position and the attachment design on the load transfer and root control remains to be examined.

Some authors have reported that only tipping and intrusion can be accomplished by RTAs.¹⁵ However, our results suggest that bodily tooth movements and torque can also be performed using Invisalign aligners, since they can deliver the necessary force systems. The effectiveness of the force transfers to the teeth and the

resulting in-vivo movements need to be investigated in a future study.

For all movement types, the measured force systems decayed above 0 N/N·mm. This might be because the aligners are manufactured slightly undersized, since patients' impressions, the resin models, and the aligners shrink slightly during the manufacturing process.

Even though constant tooth movements in Clin-Check were planned, in some cases, there was great variety among the initial force systems: differences between 1 and 15 N·mm were observed for initial moments between consecutive aligners. An aligner with a high initial force system was often followed by an aligner with a low force system in all 3 movement categories. Thus, the resulting tooth movement was not constant. The minimal measured initial force or moment in all 3 types of movement groups was a slight counterforce. This means that, for example, distalization was planned, but some aligners produced no movement or a slight mesialization of the tooth. One possible explanation for the differences in the force systems between consecutive aligners as well as the slight counterforces could be inaccuracies during the manufacturing process of the aligners. Other commercial RTA systems (eg, ClearSmile system) allow much more tooth displacement in each aligner (up to 0.5 mm)¹³ compared with the Invisalign system (up to 1° of incisor torque per 0.25 mm of translation). 16,17 Indeed, patients reported aligners with a strong fit and high forces, and aligners with a loose fit.

In our study, we used patients and not a complete experimental setup. Therefore, only the main force systems corresponding to the tooth movement (Mx for premolar derotation, My for incisor torque, and Fz for molar distalization) can be directly compared between the subgroups.

Since it is not possible to perform direct measurements of the force systems generated by appliances in all 3 planes of space, an experimental setup such as ours is common to investigate these values. In comparison with other measurement systems, the orthodontic measurement and simulation system enables measurements of the forces of the initial situation and the dynamic force progression during tooth movement. However, in our experimental setup, tooth and sensor were rigidly connected, with the shortcoming that clinical parameters such as periodontal ligaments, mastication, saliva, and soft-tissue reactions could not be simulated and considered. 18 In addition, an ideal center of resistance was used for each tooth. Furthermore, the orthodontic measurement and simulation system is based on the assumption of a linear relationship between the speed of tooth movement and the amount of applied force, which stands only limited in compliance with clinical reality.

CONCLUSIONS

- The measured forces and moments created by aligners of the Invisalign system are consistent with the literature values.
- 2. The force decay is exponential during RTA wear, independent of attachments.
- 3. Force systems differ in a series of aligners, even if a constant movement in ClinCheck is planned.
- 4. Premolar derotation should be supported with an attachment, especially if these teeth have short crowns and few undercuts. Otherwise, moment transfer from the RTA to the tooth is possible only to a limited degree.

REFERENCES

- Kesling HD. The philosophy of tooth positioning appliance. Am J Orthod 1945;31:297-304.
- 2. Ponitz RJ. Invisible retainers. Am J Orthod 1971;59:266-72.
- McNamara JA, Kramer KL, Juenker JP. Invisible retainers. J Clin Orthod 1985:19:570-8.
- 4. Sheridan JJ, LeDoux W, McMinn R. Essix retainers: fabrication and supervision for permanent retention. J Clin Orthod 1993;27:37-45.
- Wong BH. Invisalign A to Z. Am J Orthod Dentofacial Orthop 2002; 121:540-1.
- Miller RJ, Derakhshan M. The Invisalign system: case report of a patient with deep overbite, upper incisor flaring, and severe curve of Spee. Semin Orthod 2002:8:43-50.
- Min S, Hwang CJ. The effect of thickness and deflection of orthodontic thermoplastic materials on its mechanical properties. Korean J Orthod 2010;40:16-26.
- Kwon JS, Lee YK. Force delivery properties of thermoplastic orthodontic materials. Am J Orthod Dentofacial Orthop 2008;133: 228-34.
- Schuster S, Eliades G, Zinelis S, Eliades T, Bradley TG. Structural confirmation and leaching from in vitro aged and retrieved Invisalign appliances. Am J Orthod Dentofacial Orthop 2004;126:725–8.
- Hahn W, Dathe H, Fialka-Fricke J, Friecke-Zech S, Zapf A, Kubein-Meesenburg D, et al. Influence of thermoplastic appliances' thickness on the magnitude of force delivered to a maxillary central incisor during tipping. Am J Orthod Dentofacial Orthop 2009; 136:12.e1-7.
- Hahn W, Engelke B, Jung K, Dathe H, Fialka-Fricke J, Kubein-Meesenburg D, et al. Initial forces and moments delivered by removable thermoplastic appliances during rotation of an upper central incisor. Angle Orthod 2010;80:239-46.
- 12. Hahn W, Zapf A, Dathe H, Fialka-Fricke J, Fricke-Zech S, Gruber R, et al. Torquing an upper central incisor with aligners—acting forces and biomechanical principles. Eur J Orthod 2010;32:607-13.
- Barbagallo LJ, Shen G, Jones AS, Swain MV, Petocz P, Darendeliler MA. A novel pressure film approach for determining the force imparted by clear removable thermoplastic appliances. Ann Biomed Eng 2008;36:335-41.
- Vardimon AD, Robbins D, Brosh T. In-vivo von Mises strains during Invisalign treatment. Am J Orthod Dentofacial Orthop 2010;138: 399-409.

- 15. Brezniak N. The clear plastic appliance. Angle Orthod 2008;78: 381-2.
- Boyd RL. Predictability of successful orthodontic treatment using Invisalign. The Greater Philadelphia Society of Orthodontists page. Available at: http://www.gpso.org/events/2003_outline.pdf. Accessed September 1, 2007.
- Clark D. The Invisalign system—challenging movements. Available at: http://www.aligntechinstitute.com/files/ATEArchive/pdf/Chall engingMovements_10-5-07-final.pdf. Accessed May 10, 2007.
- Bourauel C, Drescher D, Thier M. An experimental apparatus for the simulation of three-dimensional movements in orthodontics. J Biomed Eng 1992;14:371-8.
- **19.** Harzer W, Bourauel C, Gmyrek H. Torque capacity of metal and polycarbonate brackets with and without a metal slot. Eur J Orthod 2004;26:435-41.
- Pedersen E, Andersen K, Gjessing PE. Electronic determination of centres of rotation produced by orthodontic force systems. Eur J Orthod 1990;12:272-80.
- 21. Ren Y, Maltha JC, Kuijpers-Jagtman AN. Optimum force magnitude for orthodontic tooth movement: a systematic literature review. Angle Orthod 2003;73:86-92.
- **22.** Sheridan JJ. The readers' corner. 2. What percentage of your patients are being treated with Invisalign appliances? J Clin Orthod 2004;38:544–5.